# EFFET OF THICKNESS OF DIFFERENT SHAPE MEMORY POLYMER LAYERS ON DAMPING PERFORMANCE

## Abstract

Unconstrained layer damping, also known as extensional damping, is a surface damping treatment for vibration suppression. This investigation utilized tensile and dynamic mechanical analysis tests and analytical studies on polyurethane, silicone, and butyl rubbers for asymmetrical and proportioned configurations. Results showed that butyl rubber provided better results in reducing vibration amplitude in rectangular and Tubular cavities. Free layered damped samples were modeled using Solid Works, and modal analysis was conducted on the ANSYS R19 workbench.

**Keywords:** Free layer damping, optimization, symmetrical and asymmetrical structure.

## Authors

# M. Prasanth Kumar

Assistant Professor Department of Civil Engineering Chaitanya Engineering College Visakhapatnam, India.

# **Betha Hemanth**

Associate Professor Department of Mechanical Engineering ANITS Visakhapatnam, India.

## I. INTRODUCTION

Material damping is the energy dissipation property of a material, converting mechanical energy into thermal energy. It is produced by friction and determined by loading and unloading phases of a process. Applying damping material on the vibrating surface are the passive methods of reducing vibration, typically associated with sheet metal structure vibration. There are two types of damping treatments: Free Layer Damping (FLD) treatment and Constrained Layer Damping (CLD). Unconstrained Layer Damping is a free-layer treatment where a coating of a damping material is applied to one or both sides of a structure.

Shape memory alloys like Polyurethane rubber, Silicone rubber, and Butyl rubber were used as damping materials in this study, as they can return from a warped shape to its original shape when induced by temperature changes. The Ross-Kerwin-Ungar (RKU) equations can predict unconstrained-layer damping treatment performance, considering the case with zero constrained-layer thickness. The constrained-layer damping treatment's performance depends on the constraining layer's geometry and type. Sandwich damping treatments achieve maximum shear strain when the constraining layer is the same type and geometry as the structure being damped.

# **II. MODAL ANALYSIS**

This study examines a FLD structure consisting of AA 6063 base metal and Epoxy Adhesive-based damping materials like polyurethane, silicone, and Butyl rubbers with 75 Shore A hardness [1].

FLD samples were created using SOLIDWORKS software, following ASTM-E756 standards. These samples were made from Polyurethane, Silicone, and Butyl rubbers with cavities in different configurations. The base plate was made of AA6063, and the layer material was glued to it using epoxy resin. The damping effect from the adhesive was ignored due to the small adhesive thickness of around 3 micron meters [2][3].

Specimen	Materials	Length (mm)	Thickness (mm)	Width (mm)
Base plate	AA6063	$L_1 = 300$	$h_1 = 3$	25.4
Layer	Polyurethane,	$L_2 = 250$	$h_2 = 30, 40, 50$	25.4
	Silicone and		(symmetric and	
	Butyl Rubbers		asymmetric)	



Figure 1: Basic Shape of FLD sample with no cavities



Figure 2: FLD beam with Tubular cavities of each 10mm diameter



Figure 3: FLD beam with rectangular cavities of size 10mm X 20mm



Figure 4: (b) Asymmetrical FLD beam- 30mm thick PU rubber coating with Tubular cavities



Figure 4: (d) Proportioned FLD beam- 30mm thick PU rubber coating with Tubular cavities



Figure 4: (a) Asymmetrical FLD beam- 30mm thick PU rubber coating with Rectangular cavities



Figure 4: (c) Proportioned FLD beam- 30mm thick PU rubber coating with Rectangular cavities



Figure 4: (f) Asymmetrical FLD beam- 30mm thick Silicone rubber coating with Tubular cavities



Figure 4: (h) Proportioned FLD beam- 30mm thick Silicone rubber coating with Tubular cavities



Figure 4: (e) Asymmetrical FLD beam- 30mm thick Silicone rubber coating with rectangular cavities



Figure 4: (g) Proportioned FLD beam- 30mm thick Butyl rubber coating with rectangular cavities









Figure 4: (1) Proportioned FLD beam- 30mm thick Butyl rubber layer with rectangular cavities



Figure 4: (i) Proportioned FLD beam- 30mm thick silicone rubber coating with rectangular cavities



Figure 4: (k) Proportioned FLD beam- 30mm thick Butyl rubber layer with Tubular cavities

Table 2 displays natural frequency values from modal analysis of Polyurethane, Silicone, and Butyl rubber under symmetrical and unsymmetrical damping of 30, 40, and 50 mm thickness [4 to 7].

				Natural	Natural
S.	Type of	Thickness	Form of	Frequency with	Frequency with
No.	SMP	(mm)	Cavity	Proportioned	Asymmetrical
				shape (Hz)	shape (Hz)
1	Polyurethane rubber	30	Rectangular	61.01	75.48
		30	Tubular	62.11	75.32
		40	Rectangular	52.73	57.19
		40	Tubular	50.08	55.97
		50	Rectangular	37.61	43.63
		50	Tubular	36.68	42.78
2	Silicone rubber	30	Rectangular	61.39	77.92
		30	Tubular	61.72	75.83
		40	Rectangular	51.85	57.85
		40	Tubular	50.59	56.62
		50	Rectangular	37.99	44.22
		50	Tubular	43.32	43.45
3		30	Rectangular	70.84	79.62
	Butyl rubber	30	Tubular	70.23	77.12
		40	Rectangular	54.98	60.77
		40	Tubular	50.79	58.96
		50	Rectangular	40.85	47.58
		50	Tubular	39.71	44.59

**Table 2: Natural frequencies of FLD beams** 

The above study reveals that increasing mass or lowering stiffness lowers natural frequency, while reducing mass or increasing stiffness increases it [8 to 10]. Asymmetrical configurations can operate at higher speeds without noise, wear, metal fatigue, or uneven performance. Modal analysis shows that asymmetrical configurations provide better resonant frequency response than symmetrical [11 to 13].

## **III.CONCLUSIONS**

This study examines the damping performance of various shape memory polymers, including Polyurethane, Silicone, and Butyl rubbers. DMA tests and modal analysis are conducted using ANSYS R19 software to determine the best damping properties of the materials. Python programming is used to determine optimal values. The results show that the unsymmetrical configuration of butyl rubber with a rectangular cavity at 79.62 Hz has better results for natural frequency.

#### REFERENCES

- [1] Prasanth Kumar M, Mamatha B, Bhaskara Raju VVS, N.Ramanaiah, (2017) "Effect of thickness on asymmetric Extensional Damping Treatment using Viscoelastic Materials". International Journal of Engineering Trends and Technology (IJETT).
- [2] N.Ramanaiah, Prasanth Kumar Mallipudi, VVS. Bhaskara Raju, *et al.* (2017) "Effectiveness of Extensional Damping using Rubber as Layer". Trends in Mechanical Engineering &Technology (TMET).
- [3] C.V.Ramachandrareddy, N.Ganesn, Narayanan.B.V "The response of plates with unconstrained layer damping treatment to random acoustic excitation" (1979).
- [4] A.D.Roberts and C.A. Brackley, "Surface treatment of rubber to reduce friction", Journal of Natural Rubber Research, Volume 4, Number 1, pp. 1-21, March (1989).
- [5] H.H.Law, P.L.Rossiter, G.P.Simon, L.L.Koss, "Characterization of mechanical vibration damping by piezoelectric materials", Journal of Sound and VibrationVolume 197, Issue4, Pages 489-513, October (1996).
- [6] Roynganesan, "The theoretical and experimental investigations on the damping effectiveness of partially applied unconstrained layer damping treatments on rectangular plates having central rectangular cutouts" (2003).
- [7] Doo-holee, Woo-Seok Hwang, "Optimization of length for unconstrained viscoelastic damping layer of beams" (2004).
- [8] Ramji Koona, Ganesh Kumar PVS and M.Lavanya "Optimization of surface damping treatments for random vibration control of structures Dynamic excitation results in vibration of machinery and supports of the structures"(2005).
- [9] Laurent hazard, "Design of viscoelastic damping for vibration and noise control, modeling, experiments and optimization" (2006).
- [10] H.H.Hilton, and Sung Yi, M. Fouad Ahmad "Dynamic Responses of Plates with Viscoelastic Free Layer Damping Treatment" journal of vibration and acoustics 362/vol.118, (2008).
- [11] Craig A.Gallimore, Dr. Kevin B.Kochersberger "Passive Viscoelastic Constrained Layer Damping Application for a Small Aircraft Landing Gear System" (2008).
- [12] Francesca Cura, Andrea Mura1 and Fabrizio Scarpa, "Modal strain energy based methods for the analysis of complex patterned free layer damped plates", Journal of Vibration and Control, 18(9) pp.1291–1302, (2011).
- [13] Ashish M. Dharme, Pravin P. Hujare and Sinhgad "Analysis of performance of FLD and CLD technique", International Journal of Engineering Sciences & Research Technology, pp.340-343, ISSN: 2277-9655, (2015).