

FORMULAE HAND BOOK FOR STRENGTH OF MATERIALS

Abstract

Formulas for Strength of Materials" is a meticulously crafted reference guide that serves as an indispensable resource for students, engineers, and professionals seeking a deep understanding of the fundamental principles governing the behavior of materials under various loads and stresses. This comprehensive compendium offers a systematic collection of equations, equations, and insights, making it a valuable asset for anyone engaged in the design, analysis, and application of structural components in engineering and construction.

In this book, the author provides a wide-ranging selection of formulas, categorized by topic, including stress analysis, strain, deformation, and the mechanical properties of materials. Each formula is accompanied by clear explanations, practical examples, and relevant diagrams, enabling readers to grasp the underlying concepts and their real-world applications.

Formulas for Strength of Materials" is a valuable addition to the library of anyone involved in mechanical and civil engineering, providing a one-stop source for essential equations and insights that empower professionals and students to tackle challenges in structural design and analysis with confidence.

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I. SIMPLE STRESS AND STRAIN

1. SIMPLE STRESS AND STRAIN FORMULAE HAND BOOK FOR STRENGTH OF MATERIALS

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Stress(σ)	$\sigma = \frac{P}{A}$	Where, σ =stress in N/mm ² P= Load in N A=Area in mm ²
Strain (e)	$e = \frac{\Delta L}{L}$	Where, e =strain ΔL = Change in length or elongation in mm L=Original length or gauge length in mm
Youngs modulus(E)	$E = \frac{\sigma}{e}$	Where, E= Youngs modulus or modulus of elasticity in N/mm ² σ =stress in N/mm ² e =strain
Factor of safety(FoS)	$FOS = \frac{\sigma_u}{\sigma}$	Where, σ_u =Ultimate stress in N/mm ² σ =Working stress in N/mm ²
Area(A)	$A = \pi/4 \times d^2$ $A = \pi/4 \times (D^2 - d^2)$ $A = b \times t$	Where, A=area in mm ² D= Major diameter or outer diameter in mm d= Minor diameter or inner diameter in mm b= breadth or wide in mm t= Thickness in mm

2. UTM (TENSILE TEST)

Yield Stress(σ_y)	$\sigma_y = \frac{P_y}{A}$	Where, σ_y = Yield stress in N/mm ² P _y = Yield Load in N A=Area in mm ²
Ultimate Stress(σ_u)	$\sigma_u = \frac{P_u}{A}$	Where, σ_u = Ultimate stress in N/mm ² P _u = Ultimate Load in N A=Area in mm ²

Breaking Stress(σ_B)	$\sigma_B = \frac{P_B}{A}$	Where, σ_B = Breaking stress in N/mm ² P_B = Breaking Load in N A =Area in mm ²
% of Elongation ($\% \Delta L$)	$\% \Delta L = \frac{(L_F - L_I)}{L_I} \times 100$	Where, L_F = Final length in mm L_I = Initial length in mm
% of Reduction area ($\% \Delta A$)	$\% \Delta A = \frac{A - a}{A} \times 100$	Where, A = Initial area in mm ² a = Final area or area of neck in mm ²

3. VOLUMETRIC STRAIN

Volumetric strain (e_v)	$e_v = \Delta V / V = e_{lin} \times (1 - 2 \times 1/m)$	Where, e_v = Volumetric strain ΔV = Change in volume in mm ³ V =Original volume in mm ³ $1/m$ = Poisson's ratio e_{lin} = Linear strain
Volume (V)	$V = A \times L$	Where, A = Area in mm ² L = Length in mm
Poisson's ratio (1/m)	$1/m = e_{Lat} / e_{lin}$	Where, e_{Lat} = Linear strain e_{Lin} = Linear strain or Longitudinal strain
Lateral strain (e_{Lat})	$e_{Lat} = \Delta d / d \text{ (or) } \Delta b / b \text{ (or) } \Delta t / t$	Where, Δd = Change in diameter in mm d = Original diameter in mm Δb = Change in breadth or width in mm b = Original breadth or width in mm Δt = Change in thickness in mm t = Original thickness in mm
Linear strain (e_{Lin})	$e_{Lin} = \Delta L / L$	Where, ΔL = Change in length or elongation in mm L =Original length or gauge length in mm

4. ELASTIC CONSTANTS (E,G &K)

Young's modulus (E)	Bulk modulus (K)	Rigidity modulus (C or N or G)
$E = \frac{\sigma}{e}$	$K = \frac{\sigma d}{eV}$	$C = N = G = \frac{\sigma S}{eS}$
Where, E= Youngs modulus or modulus of elasticity in N/mm ² σ =stress in N/mm ² e =strain	Where, K= Bulk modulus or in N/mm ² σ_d = Direct stress in N/mm ² e_v = Volumetric strain	Where, C=N=G=Modulus of rigidity or shear modulus in N/mm ² e_s = Shear strain
Relationship between E,G,K		
$E = 2G \times (1 + 1/m)$ $E = 3K \times (1 - 2 \times 1/m)$ $E = 9KG / (3K + G)$		

5. OMPOSITE BAR

Condition (i)	$P = P_1 + P_2$ $P = \sigma_1 A_1 + \sigma_2 A_2$	Where, P=Total load acting on the composite in N σ_1 =Stress induced in Material -1 σ_2 =Stress induced in Material -2 A_1 = Mareial-1 cross sectional area in mm ² A_2 = Mareial-2 cross sectional area in mm ²
Condition (ii)	$e_1 = e_2$ $\sigma_1/E_1 = \sigma_2/E_2$	Where, σ_1 =Stress induced in Material -1 σ_2 =Stress induced in Material -2 E_1 = Young's modulus of Material -1 E_2 = Young's modulus of Material -2

II. SHEAR FORCE AND BENDING MOMENT DIAGRAM

1. DIAGRAM SHORT CUT (SFD AND BMD)

LOAD	SFD	BMD
Point	Horizontal	Inclination
U.D.L	Inclination	Parabola
U.V.L	Parabola	Parabola

2. CALCULATIONS (SFC AND BMC)

BEAM	LOAD	SFC	BMC
Cantilever, Simply supported	Point	W	W×D
Cantilever, Simply supported	U.D.L	W×D	W×D×(D/2+G)
Cantilever, Simply supported	U.V.L	1/2bh	Or $\frac{1}{2} \times bh \times \left(\frac{1}{3} \times d + G\right)$ $\frac{1}{2} \times bh \times \left(\frac{2}{3} \times d + G\right)$
Where, W= Load in N or KN, D= Distance in m or mm, G= Gap in m or mm			

3. THEORY OF SIMPLE BENDING

Bending equation	$\frac{M}{I} = \frac{\sigma b}{y} = \frac{E}{R}$	Where, M=Bending moment or moment of resistance in N-mm I= Moment of inertia in mm ⁴ σ_b = Bending stress in N/mm ² y= Distance in mm E= Youngs modulus or modulus of elasticity in N/mm ² R= Radius of curvature in mm
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BEAM	LOAD	BENDING MOMENT (M)
Cantilever	Point	WL
Cantilever	U.D.L	$\frac{WL^2}{2}$
Simply supported	Point	$\frac{WL}{4}$
Simply supported	U.D.L	$\frac{WL^2}{8}$

BEAM SECTION	MOMENT OF INERTIA (I)	DISTANCE (y)	SECTION MODULUS (Z=I/y)
Solid circular	$\frac{\pi}{64} \times d^4$	d/2	$\pi/32 \times d^3$
Hollow circular	$\frac{\pi}{64} \times (D^4 - d^4)$	D/2	$\pi/32 \times (D^4 - d^4)/D$
Rectangular	$\frac{bd^3}{12}$	d/2	$bd^2/6$
Square or cube	$\frac{a^4}{12}$	a/2	$a^3/6$

4. TORSION

Torsional Equation	$T/J = f_s / R = C\theta/L$	<p>Where,</p> <p>T=Torque or twisting moment in N-mm J= Polar Moment of inertia in mm⁴ f_s = Shear stress in N/mm² R= Radius in mm C=N=G=Modulus of rigidity or shear modulus in N/mm² θ= Angle of twist in radians</p>
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Power(P)	$P = 2\pi NT / (60 \times 10^3)$	<p>Where,</p> <p>P= Power in Watts T=Torque or twisting moment in N-mm N=Speed in Rpm θ= Angle of twist in radians</p>
Torque(T)	$T = \pi/16 \times f_s \times d^3$ For solid shaft	<p>Where,</p> <p>T=Torque or twisting moment in N-mm f_s = Shear stress in N/mm² d= Diameter in mm</p>
	$T = \pi/16 \times f_s \times (D^4 - d^4/D)$ For Hollow shaft	<p>Where,</p> <p>T=Torque or twisting moment in N-mm f_s = Shear stress in N/mm² D=Major diameter in mm d= Minor Diameter in mm</p>
Polar moment of inertia (J)	$J = \pi/32 \times d^4$ For solid shaft	<p>Where,</p> <p>J=Polar moment of inertia moment in N-mm d= Diameter in mm</p>
	$J = \pi/32 \times (D^4 - d^4)$ For Hollow shaft	<p>Where,</p> <p>J=Polar moment of inertia moment in N-mm D=Major diameter in mm d= Diameter in mm</p>
Radius (R)	R=d/2 For solid shaft	<p>Where,</p> <p>d= Diameter in mm D=Major diameter in mm</p>
	R=D/2 For Hollow	

5. GEOMETRICAL SECTIONS

Centroid	$\bar{X} = \frac{a_1x_1 + a_2x_2 + a_3x_3}{a_1 + a_2 + a_3}$	Where, a ₁ = Section 1 area in mm ² a ₂ = Section 2 area in mm ² a ₃ = Section 3 area in mm ²
	$\bar{Y} = \frac{a_1y_1 + a_2y_2 + a_3y_3}{a_1 + a_2 + a_3}$	
Moment of inertia	$I_{xx} = b_1d_1^3/12 + b_2d_2^3/12 + b_3d_3^3/12 + a_1 \times (\bar{y} - y_1)^2 + a_2 \times (\bar{y} - y_2)^2 + a_3 \times (\bar{y} - y_3)^2$	
	$I_{yy} = d_1b_1^3/12 + d_2b_2^3/12 + d_3b_3^3/12 + a_1 \times (\bar{x} - x_1)^2 + a_2 \times (\bar{x} - x_2)^2 + a_3 \times (\bar{x} - x_3)^2$	
Radius of gyration	$K_{xx} = \sqrt{\frac{I_{xx}}{A}}$ $K_{yy} = \sqrt{\frac{I_{yy}}{A}}$ $A = a_1 + a_2 + a_3$	

III. CYLINDER AND SPHERICAL SHELLS

1. Cylindrical shell

Hoop stress or Circumferential stress (σ₁)	$\sigma_1 = \frac{Pd}{4t}$	Where, P= Internal Pressure in N/mm ² d= Internal diameter in mm t=Thickness of the cylinder in mm Δd= Change in diameter in mm ΔL= Change in length in mm E= Young's modulus in N/mm ² 1/m= Poisson's ratio
Longitudinal Stress (σ₂)	$\sigma_2 = \frac{Pd}{2t}$	
Maximum shear stress(τ)	$\tau = \frac{Pd}{8t}$	
Circumferential strain (e₁)	$e_1 = \frac{\Delta d}{d} = \frac{\sigma_1}{E} \times \left(1 - \frac{1}{2m}\right)$	
Longitudinal strain (e₂)	$e_2 = \frac{\Delta L}{L} = \frac{\sigma_1}{E} \times \left(\frac{1}{2} - \frac{1}{m}\right)$	
Volumetric Strain(e_v)	$e_v = \frac{\Delta V}{V} = e_2 + 2e_1$ $V = A \times L$ $A = \pi/4 \times d^2$	

2. Spherical shell

Hoop stress or Circumferential stress (σ_1)	$\sigma_1 = \frac{Pd}{4t}$	Where, P= Internal Pressure in N/mm ² d= Internal diameter in mm t=Thickness of the cylinder in mm Δd = Change in diameter in mm E= Young's modulus in N/mm ² 1/m= Poisson's ratio
Circumferential strain (e_1)	$e_1 = \frac{\Delta d}{d} = \frac{\sigma_1}{E} \times \left(1 - \frac{1}{m}\right)$	
Volumetric Strain(e_v)	$\Delta V = 3e_1 \times V$ $V = \pi/6 \times d^3$	

IV. SLOPE AND DEFLECTION OF THE BEAM

1. Double Integration Method

Beam	Load	Slope (θ)	Deflection (y)
Cantilever	Point load at free end	$\frac{WL^2}{2EI}$	$\frac{WL^3}{3EI}$
Cantilever	Point load apart from fixed and free end	$\frac{Wa^2}{2EI}$	$\frac{Wa^3}{3EI} + \frac{Wa^2}{2EI} \times (L - a)$
Cantilever	UDL distributed at entire length	$\frac{WL^3}{6EI}$	$\frac{WL^4}{8EI}$
Cantilever	UDL distributed from fixed end to "a" distance	$\frac{Wa^3}{6EI}$	$\frac{Wa^4}{8EI} + \frac{Wa^3}{6EI} \times (L - a)$
Simply supported	Point load at mid span	$\frac{WL^2}{16EI}$	$\frac{WL^3}{48EI}$
Simply Supported	UDL distributed at entire length	$\frac{WL^3}{24EI}$	$\frac{5WL^4}{384EI}$