### EFFET OF THICKNESS OF DIFFERENT SHAPE MEMORY POLYMER LAYERS ON DAMPING PERFORMANCE

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Abstract

Unconstrained layer damping, also known as extensional damping, is a surface damping treatment for vibration suppression. This investigation utilized UTM and DMA tests and analytical studies on polyurethane, silicone, and butyl rubbers for symmetrical and unsymmetrical configurations. Results showed that butyl rubber provided better results in reducing vibration amplitude in rectangular and cylindrical cavities. Extensional damped samples were modeled using Solid Works, and modal analysis was conducted on the ANSYS R19 workbench.

*Keywords: Damping, Unconstrained layer damping, Python programming, symmetrical and unsymmetrical configuration;*

1. Introduction:

Damping is the energy dissipation property of a material, converting mechanical energy into thermal energy. It is caused by friction and determined by loading and unloading phases of a process. Surface damping treatments are passive methods of reducing vibration, typically associated with sheet metal structure vibration. There are two types of damping treatments: Free Layer Damping (FLD) treatment and Constrained Layer Damping (CLD). Unconstrained Layer Damping is a free-layer treatment where a coating of a damping material is applied to one or both sides of a structure. Shape memory alloys like Polyurethane rubber, Silicone rubber, and Butyl rubber were used as damping materials in this study, as they can return from a deformed shape to its original shape when induced by temperature changes. The Ross-Kerwin-Ungar (RKU) equations can predict unconstrained-layer damping treatment performance, considering the case with zero constrained-layer thickness. The constrained-layer damping treatment's performance depends on the constraining layer's geometry and type. Sandwich damping treatments achieve maximum shear strain when the constraining layer is the same type and geometry as the structure being damped.

1. **Modal Analysis:**

This study examines a FLD structure consisting of AA 6063 base metal and Epoxy Adhesive-based damping materials like polyurethane, silicone, and Butyl rubbers with 75 Shore A hardness [1].

FLD samples were created using SOLIDWORKS software, following ASTM-E756 standards. These samples were made from Polyurethane, Silicone, and Butyl rubbers with cavities in different configurations. The base plate was made of AA6063, and the layer material was glued to it using epoxy resin. The damping effect from the adhesive was ignored due to the small adhesive thickness of around 3 micron meters [2][3].

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
| Table 1: Configuration of the FLD Specimen | | | | |
| **Specimen** | **Materials** | **Length (mm)** | **Thickness (mm)** | **Width (mm)** |
| Base plate | AA6063 | L1 = 300 | h1 = 3 | 25.4 |
| Layer | Polyurethane, Silicone and Butyl Rubbers | L2 = 250 | h2 = 30, 40, 50  (symmetric and asymmetric) | 25.4 |

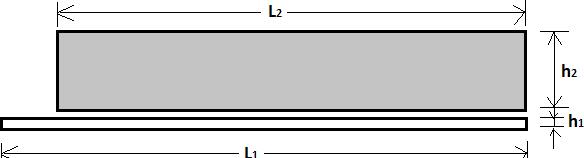


Fig.1 Configuration of FLD sample without cavities

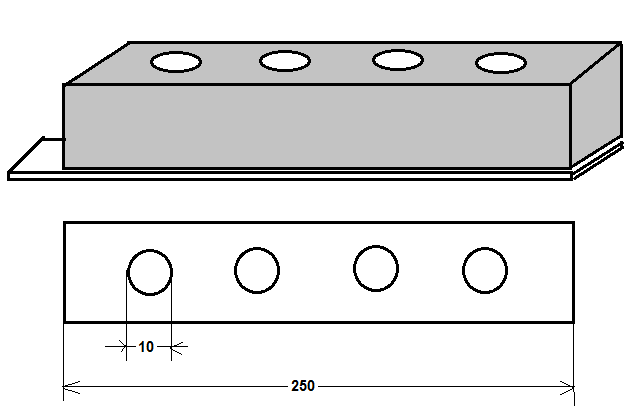


Fig.2 FLD beam with cylindrical cavities of each   
10mm diameter

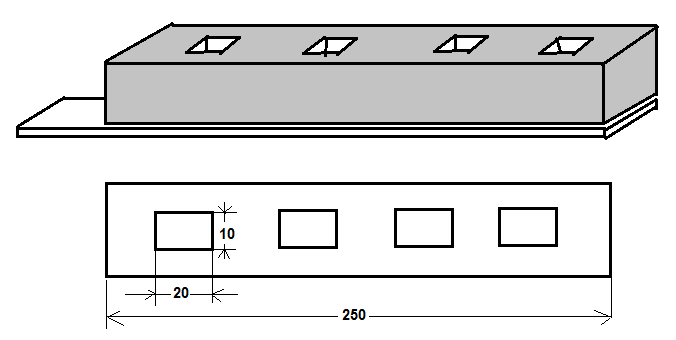


Fig.3 FLD beam with rectangular cavities of size  
10mm X 20mm

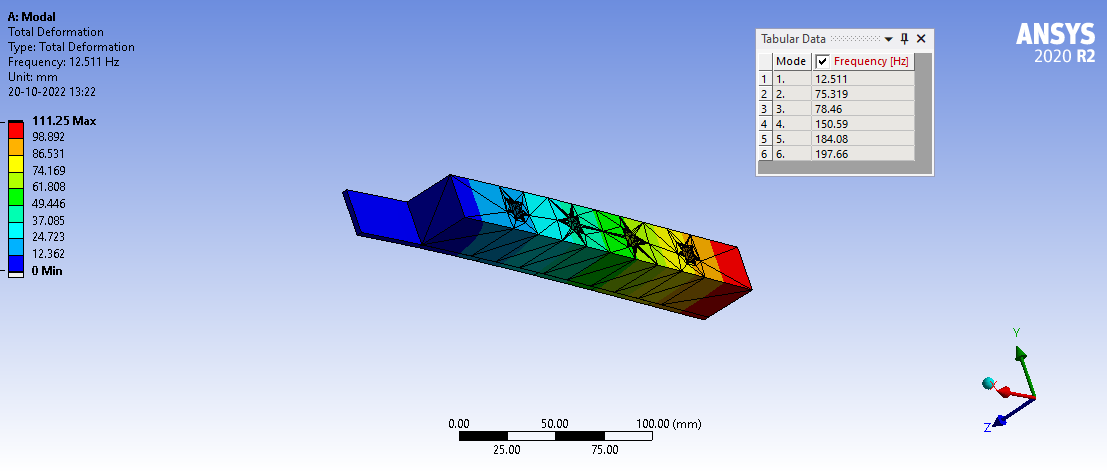
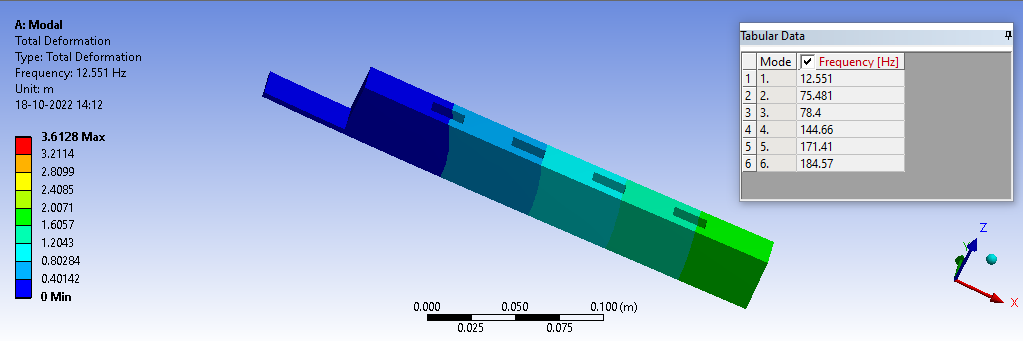


Fig.4(b) Asymmetrical FLD beam- 30mm thick PU rubber layer with cylindrical cavities

Fig.4(a) Asymmetrical FLD beam- 30mm thick PU rubber layer with Rectangular cavities

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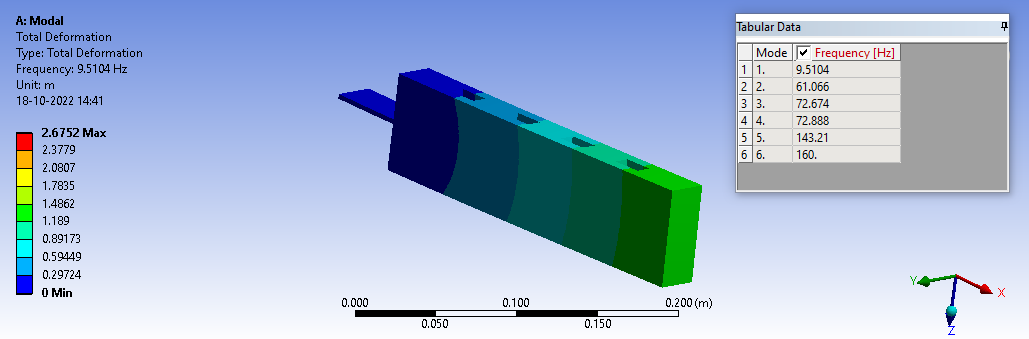
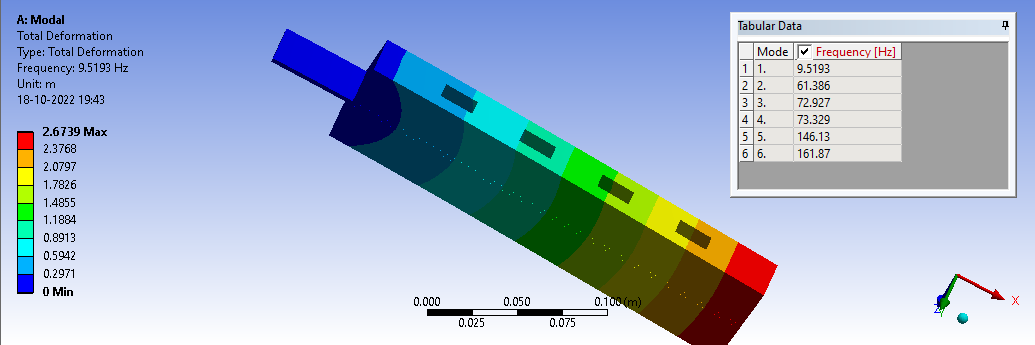


Fig.4(d) Proportioned FLD beam- 30mm thick PU rubber layer with cylindrical cavities

Fig.4(c) Proportioned FLD beam- 30mm thick PU rubber layer with Rectangular cavities

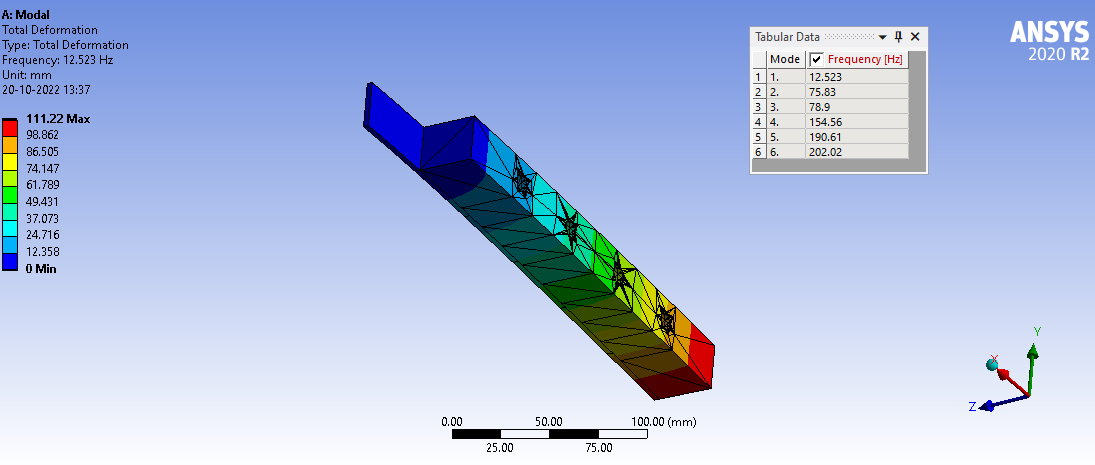
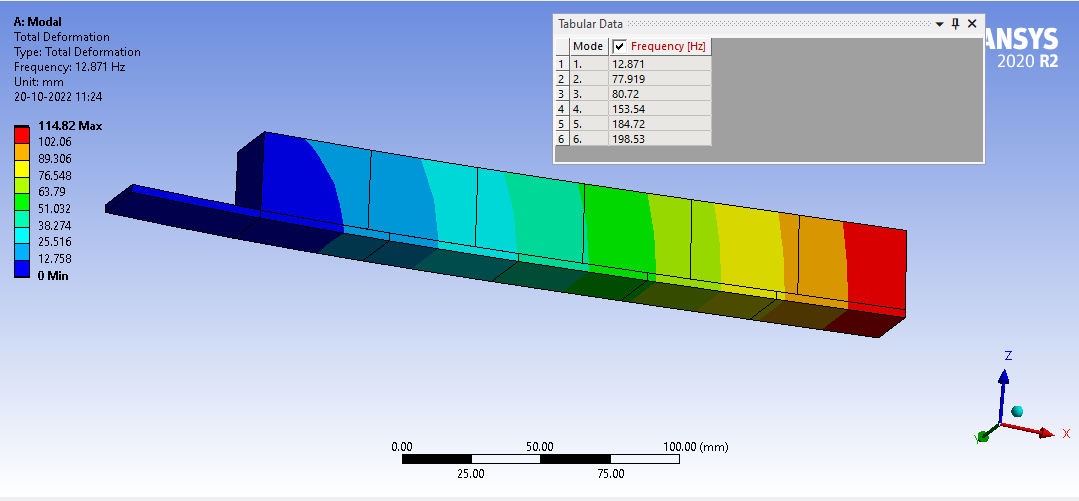


Fig.4(f) Asymmetrical FLD beam- 30mm thick Silicone rubber layer with cylindrical cavities

Fig.4(e) Asymmetrical FLD beam- 30mm thick Silicone rubber layer with rectangular cavities

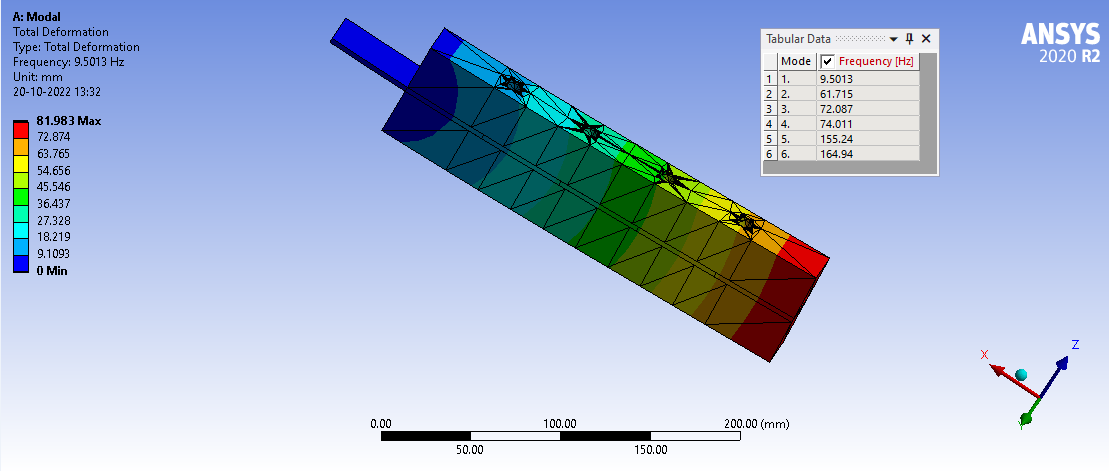
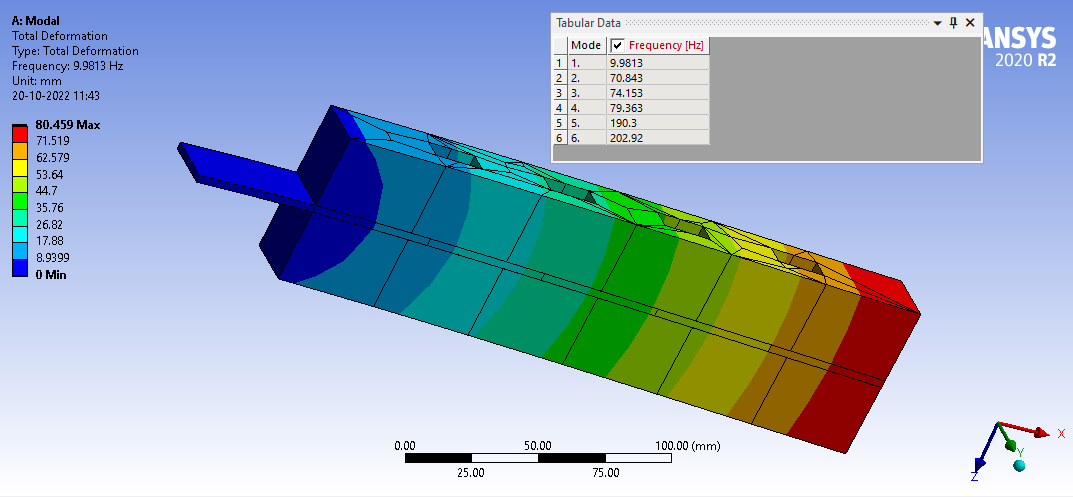


Fig.4(h) Proportioned FLD beam- 30mm thick Silicone rubber layer with cylindrical cavities

Fig.4(g) Proportioned FLD beam- 30mm thick Butyl rubber layer with rectangular cavities

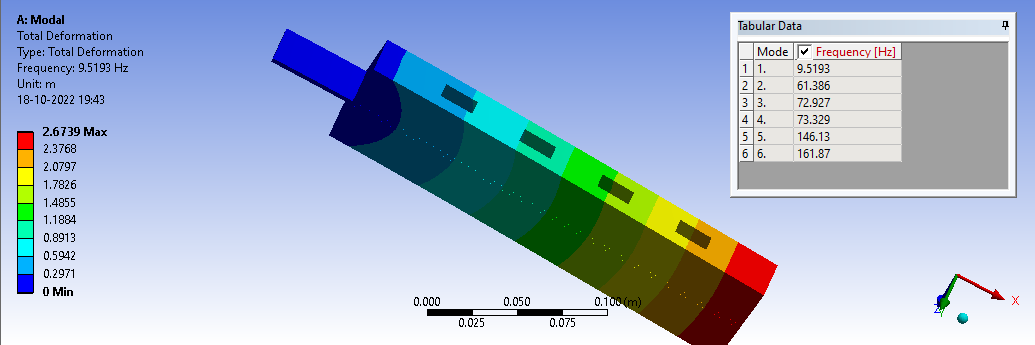
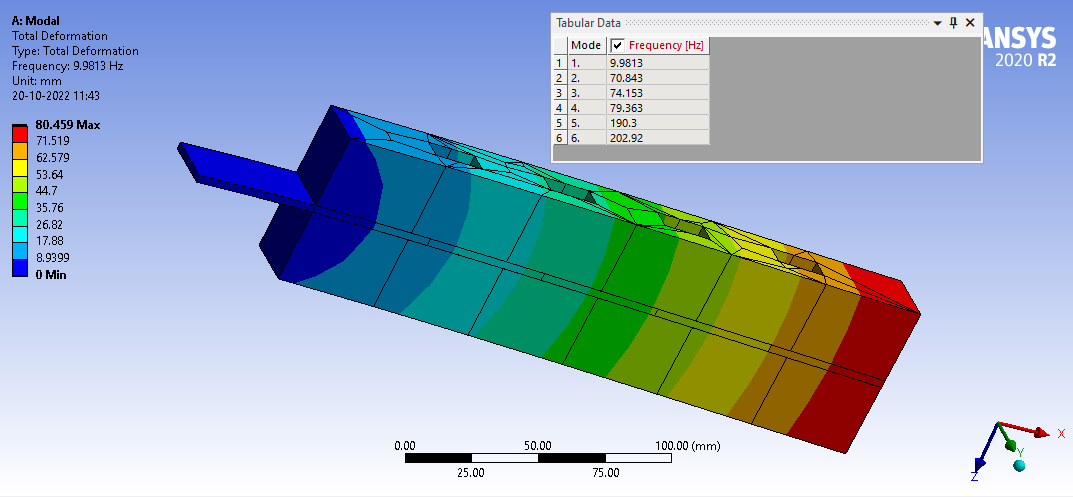


Fig.4(j) Proportioned FLD beam- 30mm thick Butyl rubber layer with rectangular cavities

Fig.4(i) Proportioned FLD beam- 30mm thick silicone rubber layer with rectangular cavities

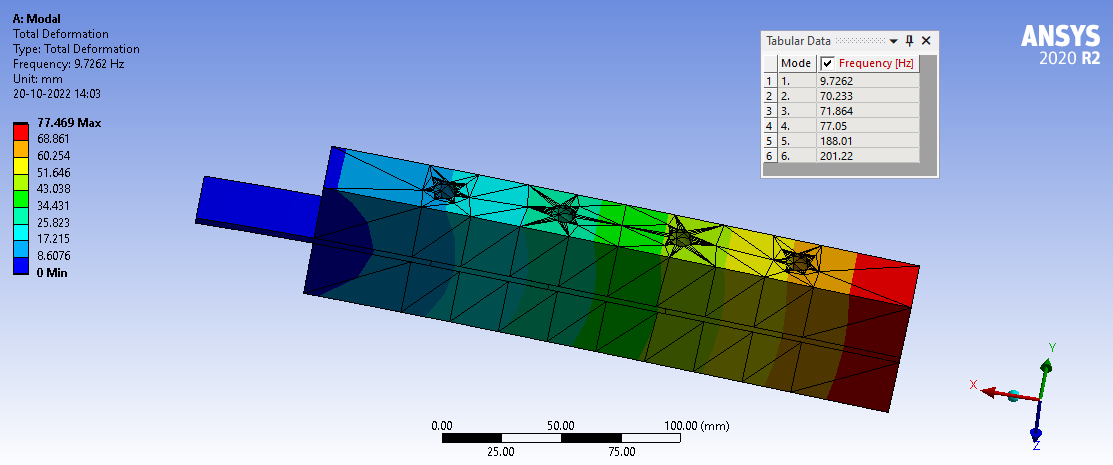
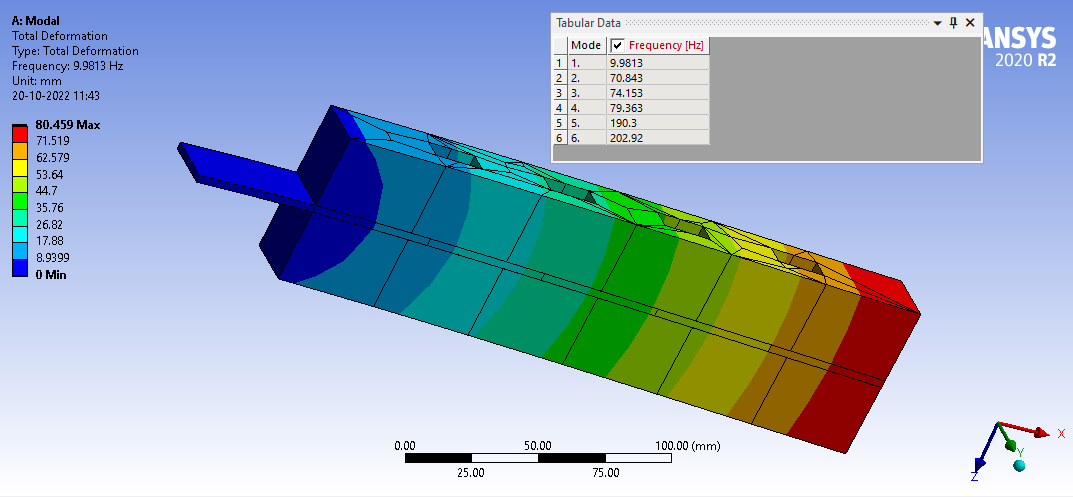


Fig.4(l) Proportioned FLD beam- 30mm thick Butyl rubber layer with rectangular cavities

Fig.4(k) Proportioned FLD beam- 30mm thick Butyl rubber layer with cylindrical cavities

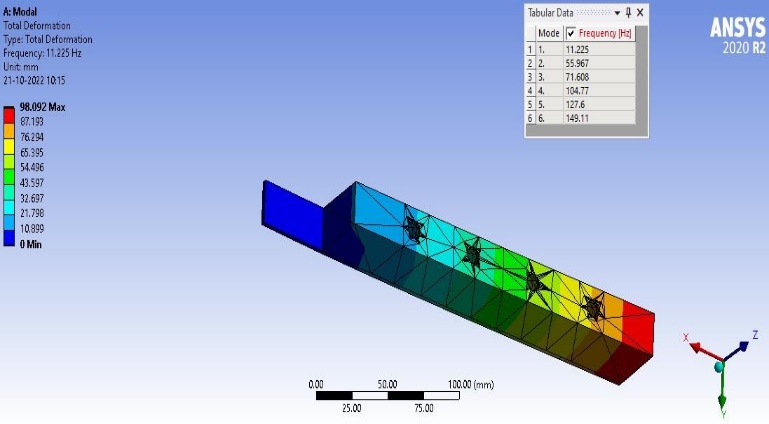
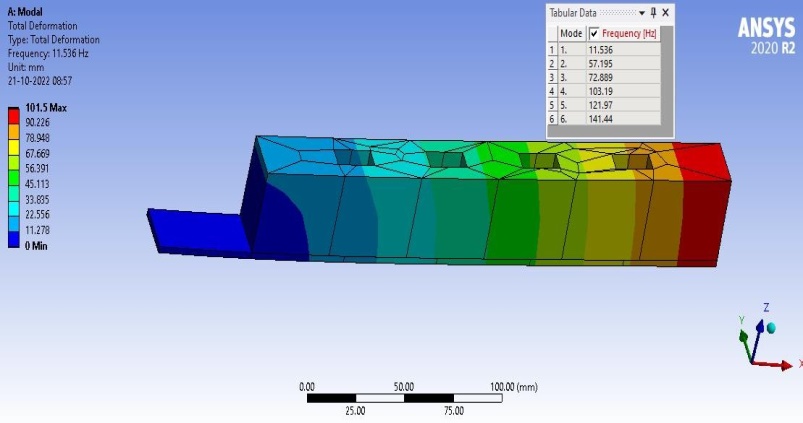


Fig.5(a) Asymmetrical FLD beam- 40mm thick PU Fig.5(b) Asymmetrical FLD beam-40mm PU



rubber layer rubber layer with Rectangular cavities with cylindrical cavity

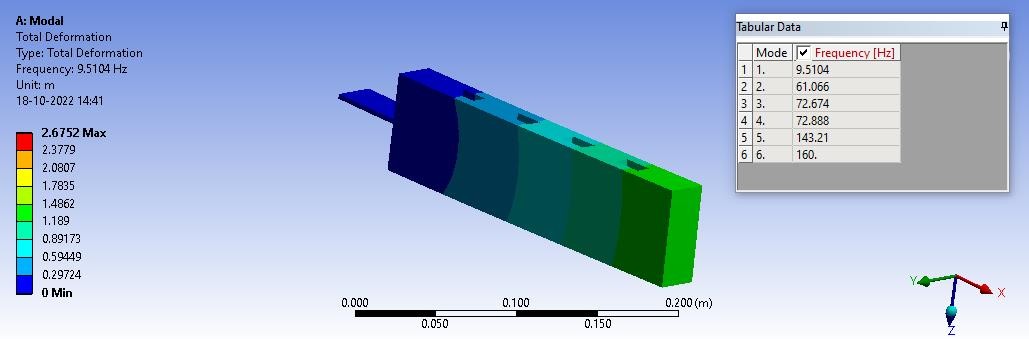
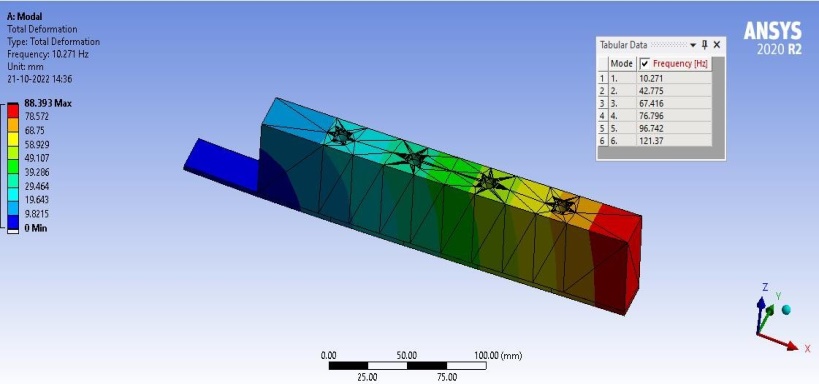


Fig.5(c) Proportioned FLD beam 40mm thick PU rubber layer Fig.5(d) Proportioned FLD beam 40mm thick PU rubber layer with rectangular cavity with cylindrical cavity

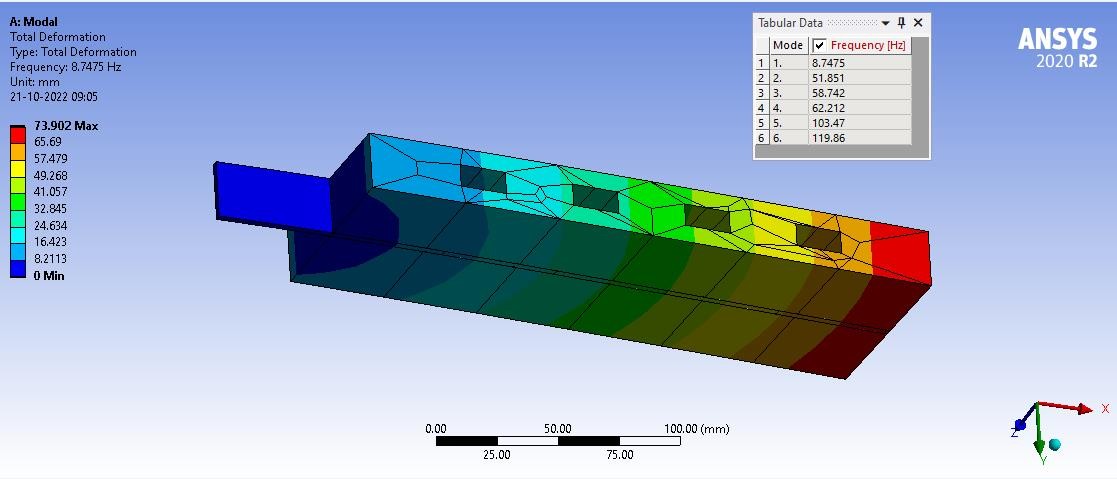
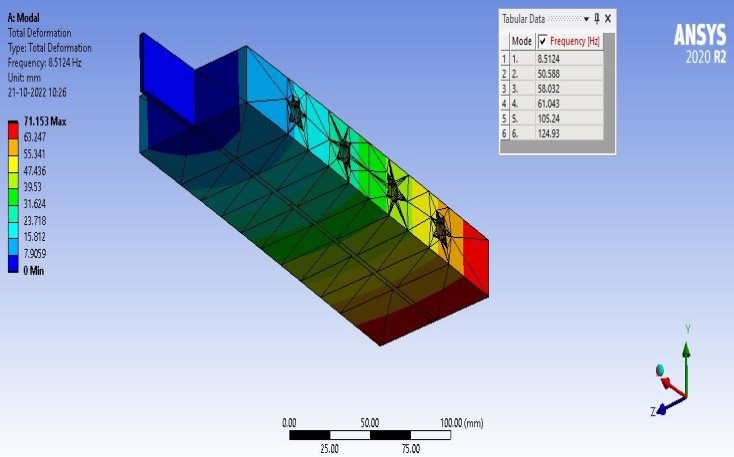


Fig.5(e) Proportioned FLD beam 40mm thick silicone rubber with Fig.5(f) Proportioned FLD beam 40mm thick Rectangular cavity silicone rubber with cylindrical cavity

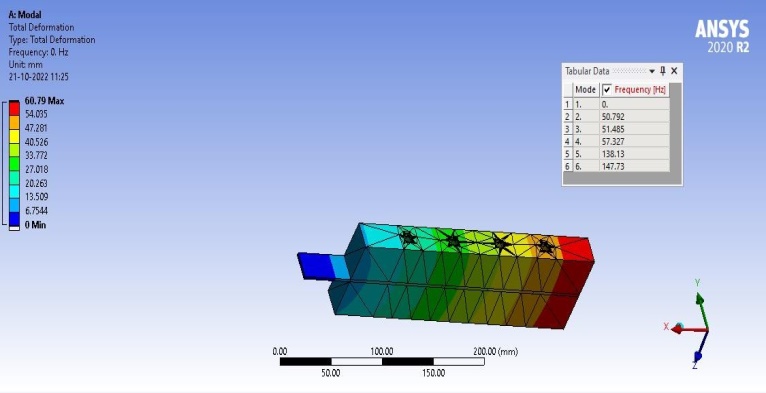
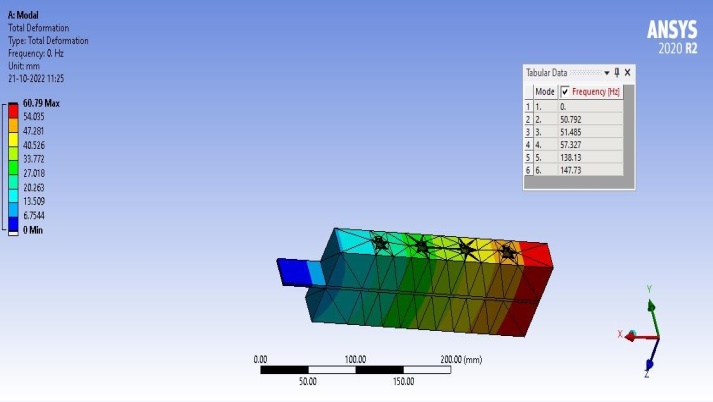


Fig.5(g) Proportioned FLD beam 40mm thick butyl rubber with Fig.5(h) Proportioned FLD beam 40mm thick butyl Cylindrical cavity rubber with cylindrical cavity

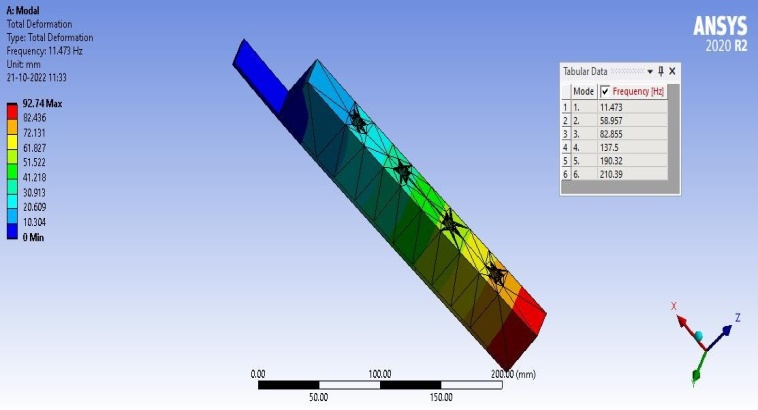
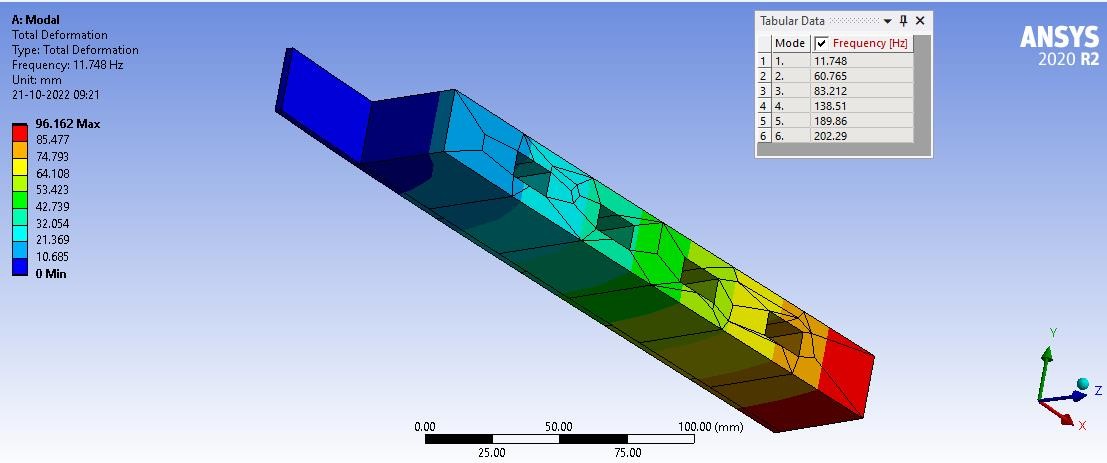


Fig.5(i) Asymmetrical FLD beam 40mm thick butyl Fig.5(j) Asymmetrical FLD beam 40mm thick butyl rubber with Rectangular cavity rubber with cylindrical cavity

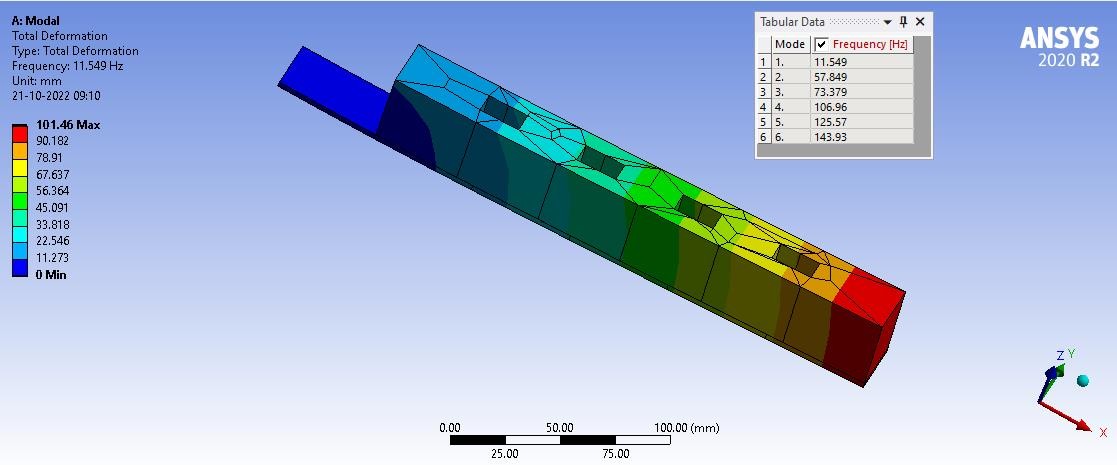
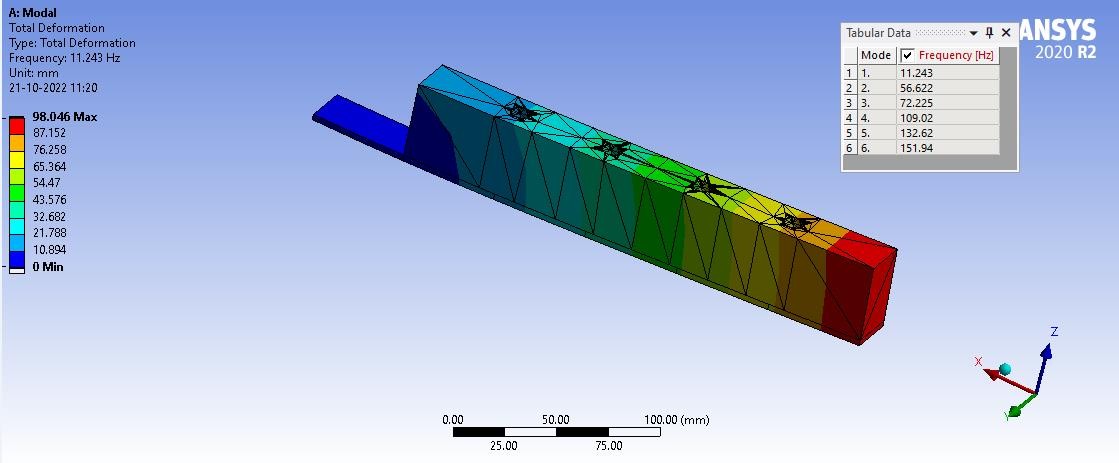


Fig.5(k) Unsymmetrical FLD beam 40mm silicone rubber with Fig.5(l) Unsymmetrical FLD beam 40mm silicone Rectangular cavity with cylindrical cavity

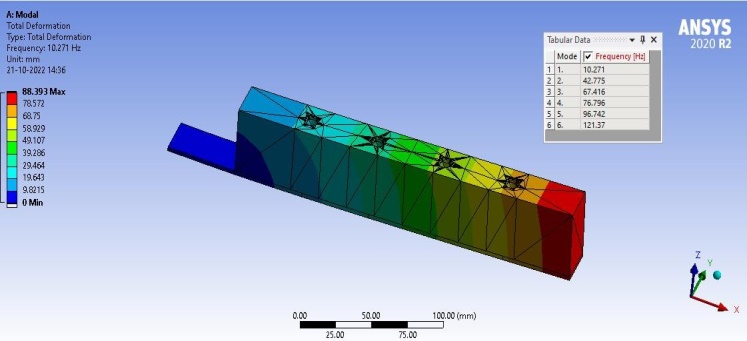
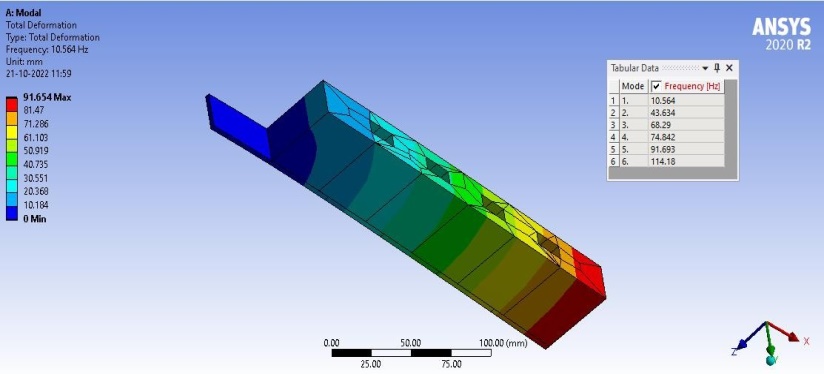


Fig.6(a) Asymmetrical FLD beam 50mm thick PU Fig.6(b) Asymmetrical FLD beam 50mm thick

Rubber with rectangular cavity PU rubber with cylindrical cavity

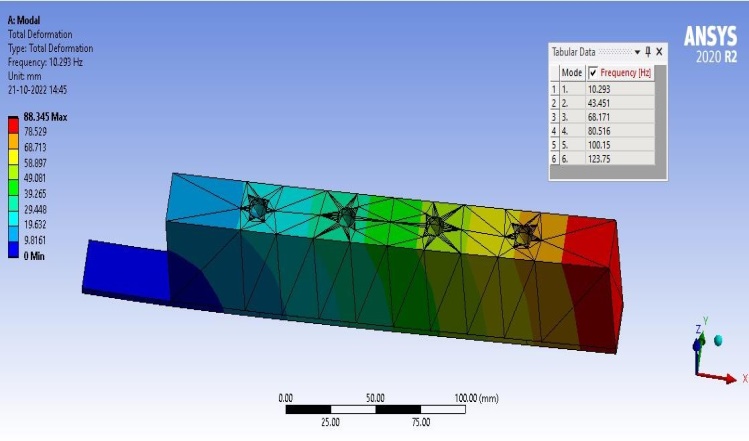
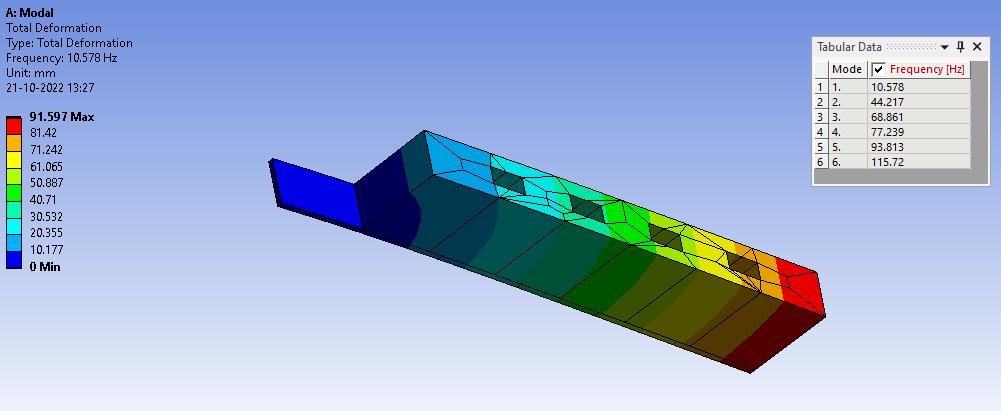


Fig.6(c) Asymmetrical FLD beam 50 mm thick silicone Fig.6(d) Asymmetrical FLD beam 50mm thick

Rubber with rectangular cavity silicone rubber with cylindrical cavity

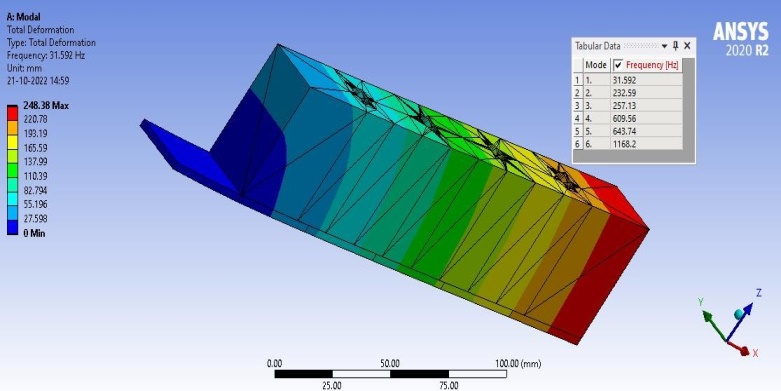
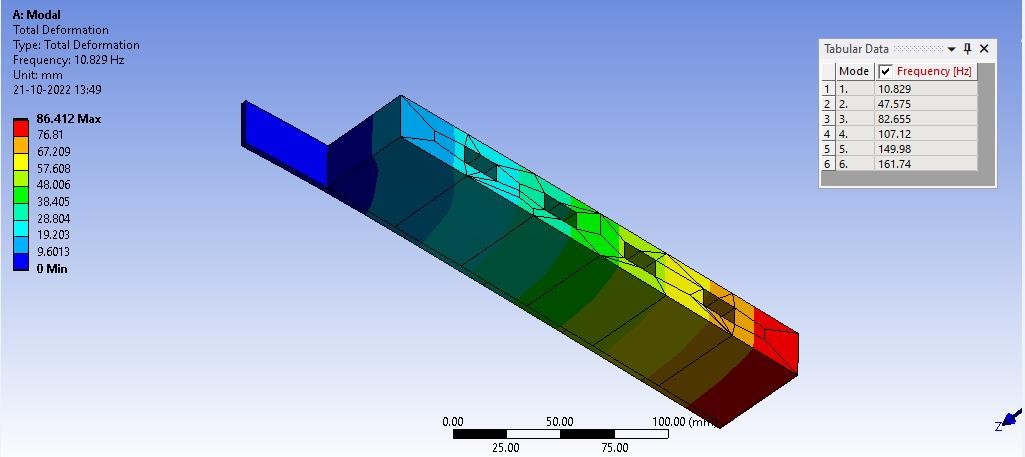


Fig.6(e) Asymmetrical FLD 50mm thick beam butyl rubber Fig.6(f) Asymmetrical FLD beam butyl rubber with Rectangular cavity with cylindrical cavity

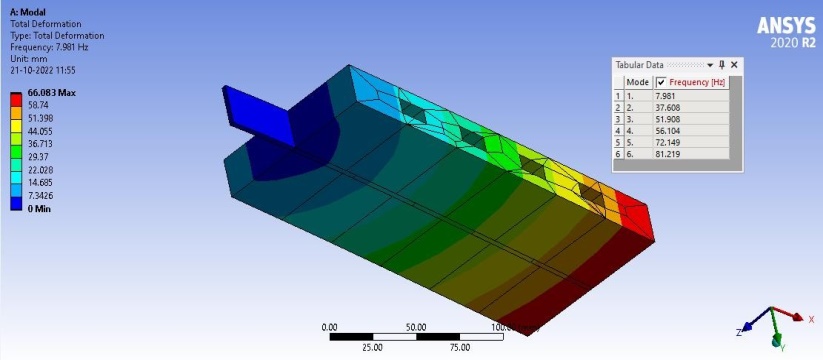
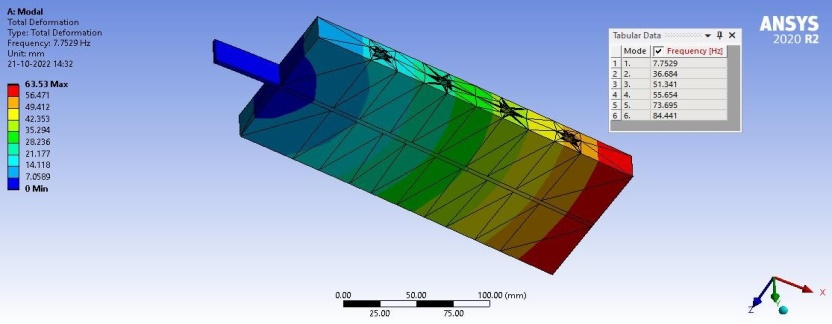


Fig.6(g) Proportioned FLD beam of 50mm PU Fig.6(h) Proportioned FLD beam of 50mm thick

rubber with rectangular cavity PU rubber with cylindrical cavity

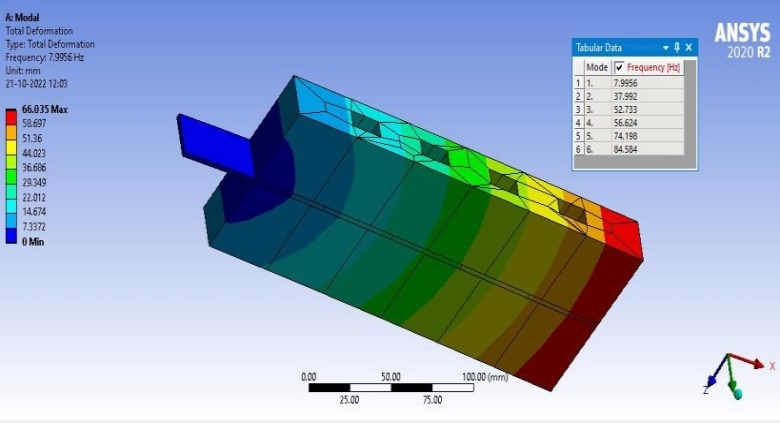
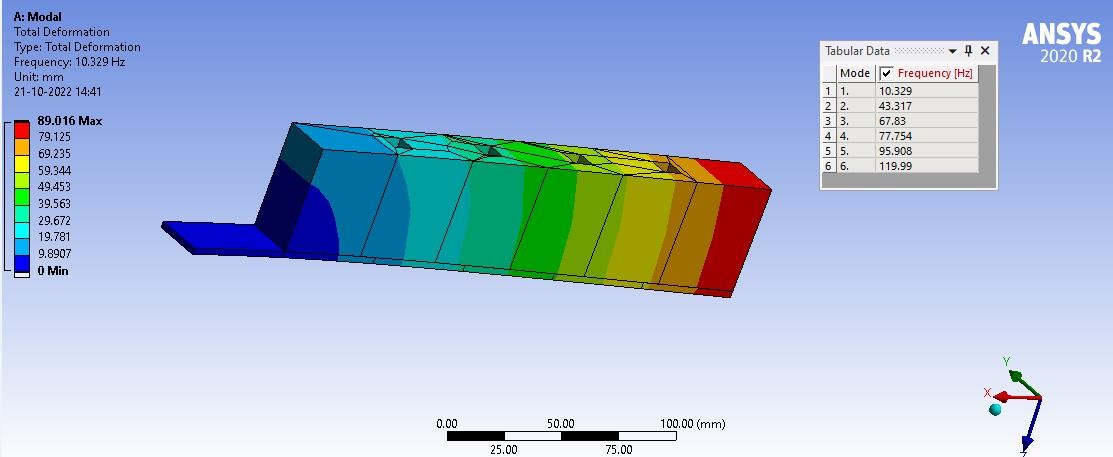


Fig.6(i) Proportioned FLD beam of 50mm silicone rubber Fig.6(j) Proportioned FLD beam of 50mm silicone

With rectangular cavity rubber with cylindrical cavity

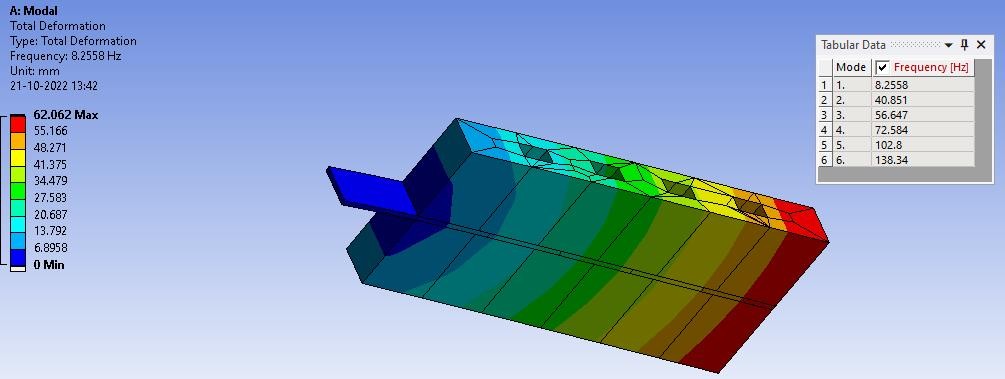
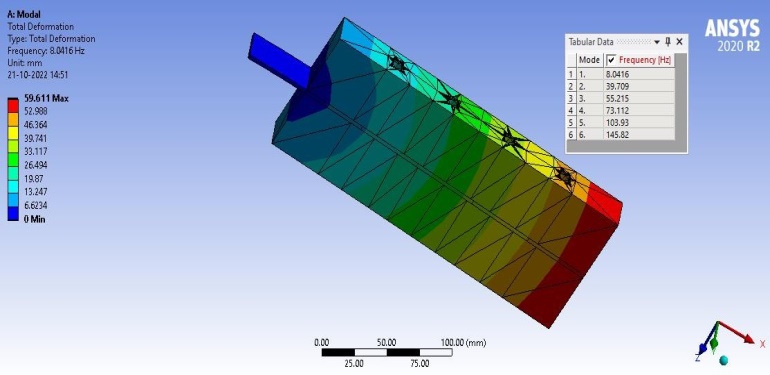


Fig.6(k) Proportioned FLD beam of 50 mm butyl rubber

With rectangular cavity Fig.6(l) Proportioned FLD beam of 50mm butyl

rubber with cylindrical cavity

Table 2 displays natural frequency values from modal analysis of Polyurethane, Silicone, and Butyl rubber under symmetrical and unsymmetrical damping of 30, 40, and 50 mm thickness [4 to 7].

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
| Table 2: Natural frequencies of FLD beams | | | | | |
| **S.No.** | **Type of**  **SMP** | **Thickness**  **(mm)** | **Shape of Cavity** | **Natural Frequency with Symmetrical configuration**  **(Hz)** | **Natural Frequency with Unsymmetrical configuration**  **(Hz)** |
| 1 | Polyurethane rubber | 30 | Rectangular | 61.01 | 75.48 |
| 30 | cylindrical | 62.11 | 75.32 |
| 40 | Rectangular | 52.73 | 57.19 |
| 40 | cylindrical | 50.08 | 55.97 |
| 50 | Rectangular | 37.61 | 43.63 |
| 50 | cylindrical | 36.68 | 42.78 |
| 2 | Silicone rubber | 30 | Rectangular | 61.39 | 77.92 |
| 30 | cylindrical | 61.72 | 75.83 |
| 40 | Rectangular | 51.85 | 57.85 |
| 40 | cylindrical | 50.59 | 56.62 |
| 50 | Rectangular | 37.99 | 44.22 |
| 50 | cylindrical | 43.32 | 43.45 |
| 3 | Butyl rubber | 30 | Rectangular | 70.84 | 79.62 |
| 30 | cylindrical | 70.23 | 77.12 |
| 40 | Rectangular | 54.98 | 60.77 |
| 40 | cylindrical | 50.79 | 58.96 |
| 50 | Rectangular | 40.85 | 47.58 |
| 50 | cylindrical | 39.71 | 44.59 |

The study reveals that increasing mass or lowering stiffness lowers natural frequency, while reducing mass or increasing stiffness increases it [8 to 10]. Unsymmetrical configurations can operate at higher speeds without noise, wear, metal fatigue, or erratic performance. Modal analysis shows that unsymmetrical configurations provide better resonant frequency response [11 to 13].

**CONCLUSIONS**

This study examines the damping performance of various shape memory polymers, including Polyurethane, Silicone, and Butyl rubbers. DMA tests and modal analysis are conducted using ANSYS R19 software to determine the best damping properties of the materials. Python programming is used to determine optimal values. The results show that the unsymmetrical configuration of butyl rubber with a rectangular cavity at 79.62Hz has better results for natural frequency.

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