

Qualitative analysis of a prey predator model with Holling type 1 and Holling type 2 functional response and non-linear prey and predator harvesting

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1 Abstract

In this paper we proposed a prey predator model to study systematically the dynamical properties of the model with non-linear prey and predator harvesting . Here we have shown that the system is positive and uniformly bounded by applying mathematical tools. We also obtained equilibrium points and analyzed bifurcations at these equilibrium points. The existence and stability of interior equilibrium point are analyzed. Saddle-node , transcritical , and hopf bifurcation are shown in this paper by varying values of parameter. Here we analyzed local and global stability and got different conditions to see the system are stable or not at equilibrium points.. In this paper we also have shown the permanence of the system under obtained condition. Numerical simulations using MATLAB are carried out as supporting evidences of our analytical findings. The main purpose of the present work is to offer a complete mathematical analysis for the model.

2 Introduction

Volterra proposed a prey predator model under the assumptions: (1) prey grows logistically in absence of predators, (2) in the absence of prey , predators die exponentially and (3) the biomass at which a predator consumes prey is a linear function of prey density. The model with the above assumption is given by

$$\frac{dx}{dt} = rx\left(1 - \frac{x}{k}\right) - axy \quad (1)$$

$$\frac{dy}{dt} = may - dy \quad (2)$$

Where x and y denote the prey and predator density respectively at time t . r and k are intrinsic growth rate and environmental carrying capacity for prey population. a is the encounter rate at which predators kill prey, m is the conversion rate of eaten prey into new predators. d is the natural death rate of predators. There are basically three types of harvesting: (1) Constant harvesting where a constant number of individuals are harvested per unit time, (2) Proportional harvesting

$$H(y) = qEy \quad (3)$$

Which means the number of individuals harvested per unit time is proportional to current population. (3) (Holling Type 2) nonlinear harvesting

$$H(y) = \frac{qEy}{m_1E + m_2y} \quad (4)$$

Where q is the catchability coefficient, E is the effort, m_1 and m_2 are suitable positive constants.

In this section we proposed a prey predator model

$$\begin{aligned} \frac{dx}{dt} &= rx\left(1 - \frac{x}{k}\right) - c_1xy - \frac{c_2xy}{a+x} - d_1x^2 - q_1Ex \\ \frac{dy}{dt} &= mc_1xy + \frac{mc_2xy}{a+x} - d_2y^2 - dy - q_2Ey \end{aligned} \quad (5)$$

subject to positive initial conditions

$$x(0) > 0, y(0) > 0 \quad (6)$$

Here $x(t)$ and $y(t)$ are prey and predator density at time t . Where r and k are intrinsic growth rate and environmental carrying capacity for prey population respectively. c_1 is the encounter rate of at which predators kill prey, m is the conversion rate of eaten prey into new predators. c_2 is the maximum value of the per capita reduction rate of prey. a measures the extent to which the environment provides protection to prey and predator. d_1 , and d_2 are the intraspecific competition for prey and predator respectively. All the parameters are assumed to be positive due to biological considerations,

3 Mathematical analysis

3.1 Positivity

Theorem 1. *All solutions $(x(t), y(t))$ of system (9) with initial condition (6) are positive for all $t \geq 0$.*

Proof. From the first equation of (9), after integrating it is obtained that

$$x(t) = x(0) \exp\left[\int_0^t \left\{r\left(1 - \frac{x(s)}{k}\right) - c_1y(s) - \frac{c_2y(s)}{a+x(s)} - d_1x(s) - q_1E\right\} ds\right] > 0$$

Since $x(0) > 0$

Similarly by integrating the second equation of (9) we get that

$$y(t) = y(0) \exp\left[\int_0^t \left\{ mc_1 x(s) + \frac{mc_2 x(s)}{a + x(s)} - d_2 y(s) - d - q_2 E \right\} ds\right] > 0$$

as $y(0) > 0$

Hence all solutions starting from an interior of the first quadrant remain in it for all future time. \square

3.2 Boundedness

Theorem 2. *All solutions $(x(t), y(t))$ of system (9) with initial condition (6) are uniformly bounded.*

Proof. Let us consider

$$W(t) = x(t) + \frac{1}{m}y(t)$$

Then the time derivative along the solutions of system (9) is given by

$$\frac{dW}{dt} + H_1 W \leq rx + H_1 x + \frac{H_1}{m}y$$

Now considering

$$rx + H_1 x + \frac{H_1}{m}y = H_2$$

We get

$$\frac{dW}{dt} + H_1 W \leq H_2$$

Therefore

$$0 \leq \lim_{t \rightarrow \infty} W(t) \leq \frac{H_2}{H_1}$$

as $t \rightarrow \infty$

Hence all solutions of (9) initiating from \mathbb{R}_+^2 are confined in the region $R = \{(x, y) \in \mathbb{R}_+^2 : 0 < x(t) + \frac{1}{m}y(t) < H_2 + \phi, \text{ for any } \phi > 0\}$ This proves the result for uniform boundedness of solutions of system (9). \square

4 Equilibria

In order to find the equilibria of the system (9), we consider

$$\frac{dx}{dt} = 0 \tag{7}$$

$$\frac{dy}{dt} = 0 \tag{8}$$

By simple calculation we get the axial equilibria of the system (9) as follows:

- (1) Trivial equilibrium point $E_0 = (0, 0)$
- (2) Predator free equilibrium point $E_1 = (x_1, 0)$ where

$$x_1 = \frac{r - q_1 E}{\frac{r}{k} + d_1}$$

which exist if $r > q_1 E$

- (3) interior equilibrium point $E_*(x_*, y_*)$

where x_* and y_* satisfies the following system of equation:

$$\begin{aligned} \frac{dx}{dt} &= rx\left(1 - \frac{x}{k}\right) - c_1xy - \frac{c_2xy}{a+x} - d_1x^2 - q_1Ex = 0 \\ \frac{dy}{dt} &= mc_1xy + \frac{mc_2xy}{a+x} - d_2y^2 - dy - q_2Ey = 0 \end{aligned}$$

4.1 Local stability analysis

The Jacobian matrix for system is

$$J = \begin{pmatrix} r - \frac{2rx}{k} - c_1y - \frac{ac_2y}{(a+x)^2} - 2d_1x - q_1E & -c_1x - \frac{c_2x}{a+x} \\ mc_1y + \frac{amc_2y}{(a+x)^2} & mc_1x + \frac{mc_2x}{a+x} - 2d_2y - d - q_2E \end{pmatrix}$$

So here

$$tr(J) = r - \frac{2rx}{k} - c_1y - \frac{ac_2y}{(a+x)^2} - 2d_1x - q_1E + mc_1x + \frac{mc_2x}{a+x} - 2d_2y - d - q_2E$$

and

$$\begin{aligned} det(J) &= \left(r - \frac{2rx}{k} - c_1y - \frac{ac_2y}{(a+x)^2} - 2d_1x - q_1E\right) \left(mc_1x + \frac{mc_2x}{a+x} - 2d_2y - d - q_2E\right) \\ &\quad - \left(-c_1x - \frac{c_2x}{a+x}\right) \left(mc_1y + \frac{amc_2y}{(a+x)^2}\right) \end{aligned}$$

So if

$|det(J)| < 1$ then the system is dissipative dynamical system and if $|det(J)| = 1$ then the system is conservative dynamical system, and is an undissipated system otherwise

4.1.1 Stability and dynamic behaviour of E_0

At $E_0(0, 0)$

$$J_{E_0} = \begin{pmatrix} r - q_1E & 0 \\ 0 & -d - q_2E \end{pmatrix} \text{ Therefore}$$

$E_0(0, 0)$ is

- (a) sink if $|r - q_1E| < 1$ and $|-d - q_2E| < 1$
- (b) source if $|r - q_1E| > 1$ and $|-d - q_2E| > 1$
- (c) saddle if $|r - q_1E| > 1$ and $|-d - q_2E| < 1$, or $|r - q_1E| < 1$ and $|-d - q_2E| > 1$
- (d) Non-hyperbolic if $|r - q_1E| = 1$ or $|-d - q_2E| = 1$

4.1.2 Stability and dynamic behaviour of E_1

At $E_1(x_1, 0)$

$$J_{E_1} = \begin{pmatrix} r - \frac{2rx_1}{k} - 2d_1x_1 - q_1E & -c_1x_1 - \frac{c_2x_1}{a+x_1} \\ 0 & mc_1x_1 + \frac{mc_2x_1}{a+x_1} - d - q_2E \end{pmatrix}$$

So here we get the two eigen values which are

$$r - \frac{2rx_1}{k} - 2d_1x_1 - q_1E \text{ and } mc_1x_1 + \frac{mc_2x_1}{a+x_1} - d - q_2E$$

So $E_1(x_1, 0)$ is a

- (a) sink if $|r - \frac{2rx_1}{k} - 2d_1x_1 - q_1E| < 1$ and $|mc_1x_1 + \frac{mc_2x_1}{a+x_1} - d - q_2E| < 1$
- (b) Source if $|r - \frac{2rx_1}{k} - 2d_1x_1 - q_1E| > 1$ and $|mc_1x_1 + \frac{mc_2x_1}{a+x_1} - d - q_2E| > 1$
- (c) Saddle if $|r - \frac{2rx_1}{k} - 2d_1x_1 - q_1E| > 1$ and $|mc_1x_1 + \frac{mc_2x_1}{a+x_1} - d - q_2E| < 1$
- or $|r - \frac{2rx_1}{k} - 2d_1x_1 - q_1E| < 1$ and $|mc_1x_1 + \frac{mc_2x_1}{a+x_1} - d - q_2E| > 1$
- (d) Non-hyperbolic if $|r - \frac{2rx_1}{k} - 2d_1x_1 - q_1E| = 1$ or $|mc_1x_1 + \frac{mc_2x_1}{a+x_1} - d - q_2E| = 1$

4.1.3 Dynamical behaviour of interior equilibrium point $E^*(x^*, y^*)$

At $E^*(x^*, y^*)$

$$J_{E^*} = \begin{pmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{pmatrix}$$

Where

$$\begin{aligned} M_{11} &= r - \frac{2rx^*}{k} - c_1y^* - \frac{ac_2y^*}{(a+x^*)^2} - 2d_1x^* - q_1E \\ M_{12} &= -c_1x^* - \frac{c_2x^*}{a+x^*} \\ M_{21} &= mc_1y^* + \frac{amc_2y^*}{(a+x^*)^2} \\ M_{22} &= mc_1x^* + \frac{mc_2x^*}{a+x^*} - 2d_2y^* - d - q_2E \end{aligned}$$

Here $T = tr(J_{E^*}) = M_{11} + M_{22}$ and $D = det(J_{E^*}) = M_{11}M_{22} - M_{12}M_{21}$

If $1 - T + D > 0$, then interior equilibrium point is a

- (a) Sink if $1 + T + D > 0$ and $D < 1$
- (b) Source if $1 + T + D > 0$ and $D > 1$
- (c) Saddle if $1 + T + D < 0$
- (d) Non-hyperbolic if $1 + T + D = 0$ and $T \neq 0$ or $T^2 - 4D < 0$ and $D = 1$

4.2 Global Stability Analysis

Theorem 3. *The positive interior equilibrium point is globally asymptotically stable if*

$$\frac{c_2}{(a+x_*)^2} < \frac{r}{y_*k} + \frac{d_1}{y_*} + \frac{d_2}{x_*} \quad (9)$$

Proof. To prove the global stability of positive interior equilibrium point $E_*(x_*, y_*)$ we construct a function $L(x, y) = \frac{1}{xy}$

Clearly $L > 0$ if $x > 0$ and $y > 0$.

Let,

$$\begin{aligned} h_1(x, y) &= rx\left(1 - \frac{x}{k}\right) - c_1xy - \frac{c_2xy}{a+x} - d_1x^2 - q_1Ex \\ h_2(x, y) &= mc_1xy + \frac{mc_2xy}{a+x} - d_2y^2 - dy - q_2Ey \end{aligned}$$

So,

$$\frac{\partial(h_1L)}{\partial x} + \frac{\partial(h_2L)}{\partial y} = \frac{-r}{yk} + \frac{c_2}{(a+x)^2} - \frac{d_1}{y} - \frac{d_2}{x} \quad (10)$$

So if at $E_*(x_*, y_*)$

$$\frac{\partial(h_1L)}{\partial x} + \frac{\partial(h_2L)}{\partial y} < 0$$

that is if

$$\frac{-r}{y_*k} + \frac{c_2}{(a+x_*)^2} - \frac{d_1}{y_*} - \frac{d_2}{x_*} < 0$$

Then $E_*(x_*, y_*)$ is globally asymptotically stable □

4.3 Permanence

Theorem 4. *The system (9) is permanent if*

$$(a) p_1(r - q_1E) + p_2(-d - q_2E) > 0$$

$$(b) p_1\left[r - \frac{rx_1}{k} - d_1x_1 - q_1E\right] + p_2\left[mc_1x_1 + \frac{mc_2x_1}{a+x_1} - d - q_2E\right] > 0$$

$$(c) p_1\left[r\left(1 - \frac{x_2}{k}\right) - c_1y_2 - \frac{c_2y_2}{a+x_2} - d_1x_2 - q_1E\right] + p_2\left[mc_1x_2 + \frac{mc_2x_2}{a+x_2} - d_2y_2 - d - q_2E\right] > 0$$

Proof. Let the average Lyapunov function for system (9) be

$$\sigma(x, y) = x_1^{p_1}y_2^{p_2} \quad (11)$$

Clearly, $\sigma(x, y)$ is a non-negative C^1 function defined in \mathbb{R}_+^2 and each p_i is assumed to be positive. Then

$$\psi(x, y) = \frac{\dot{\sigma}(x, y)}{\sigma(x, y)} \quad (12)$$

$$= p_1 \frac{\dot{(x)}}{x} + p_2 \frac{\dot{(y)}}{y} \quad (13)$$

$$= p_1\left[r\left(1 - \frac{x}{k}\right) - c_1y - \frac{c_2y}{a+x} - d_1x - q_1E\right] + p_2\left[mc_1x + \frac{mc_2x}{a+x} - d_2y - d - q_2E\right]$$

At $E_0(0, 0)$

$$\psi(x, y) = p_1(r - q_1E) + p_2(-d - q_2E) \quad (15)$$

At $E_1(x_1, 0)$

$$\Psi(x, y) = p_1\left[r - \frac{rx_1}{k} - d_1x_1 - q_1E\right] + p_2\left[mc_1x_1 + \frac{mc_2x_1}{a+x_1} - d - q_2E\right] \quad (16)$$

At $E_2(x_2, y_2)$

$$\psi(x, y) = p_1\left[r\left(1 - \frac{x_2}{k}\right) - c_1y_2 - \frac{c_2y_2}{a+x_2} - d_1x_2 - q_1E\right] + p_2\left[mc_1x_2 + \frac{mc_2x_2}{a+x_2} - d_2y_2 - d - q_2E\right] \quad (17)$$

Therefore if at $E_0(0, 0)$, $E_1(x_1, 0)$ and $E_2(x_2, y_2)$
 $\psi(x, y) > 0$, that is if

$$p_1(r - q_1E) + p_2(-d - q_2E) > 0 \quad (18)$$

$$p_1\left[r - \frac{rx_1}{k} - d_1x_1 - q_1E\right] + p_2\left[mc_1x_1 + \frac{mc_2x_1}{a+x_1} - d - q_2E\right] > 0 \quad (19)$$

$$p_1\left[r\left(1 - \frac{x_2}{k}\right) - c_1y_2 - \frac{c_2y_2}{a+x_2} - d_1x_2 - q_1E\right] + p_2\left[mc_1x_2 + \frac{mc_2x_2}{a+x_2} - d_2y_2 - d - q_2E\right] > 0 \quad (20)$$

Then the system is permanent. \square

5 Bifurcation

5.1 Transcritical and Saddle node bifurcation

In this subsection, we are interested in transcritical bifurcation of system (9) using Sotomayor's theorem.

Theorem 5. (1) System (9) undergoes a transcritical bifurcation around $E_0(0, 0)$ if $r - q_1E = 0$

(2) System (9) undergoes transcritical bifurcation around $E_1(x_1, 0)$ if $x_1 = k$ and $x_1 \neq \frac{k}{2}$, and saddle node bifurcation if $x_1 \neq k$.

Proof. (1) To prove that the model (9) undergoes a transcritical bifurcation around $E_0(0, 0)$, We use Sotomayor's theorem by considering r as the bifurcation parameter.

At $E_0(0, 0)$

$$J_{E_0} = \begin{pmatrix} r - q_1E & 0 \\ 0 & -d - q_2E \end{pmatrix}. \quad (21)$$

According to Sotomayor's theorem at $E_0(0, 0)$ transcritical bifurcation occurs if one of the eigen values of the jacobian at $E_0(0, 0)$ must be zero and the other

eigen value must have negative real part i.e if $r = q_1 E$. Here

$$F_r E_0 = \begin{pmatrix} x - \frac{x^2}{k} \\ 0 \end{pmatrix}$$

So at $E_0(0, 0)$

$$F_r E_0 = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

So

$$W^T F_r E_0 = 0$$

Let V and W are eigen vectors corresponding to zero eigen value of $J(E_0)$ and $J(E_0)^T$ respectively. After simple calculation we get

$$V = \begin{pmatrix} v_1 \\ v_2 \end{pmatrix} \equiv \begin{pmatrix} 1 \\ 0 \end{pmatrix} \quad (22)$$

Similarly, we get

$$W = \begin{pmatrix} w_1 \\ w_2 \end{pmatrix} \equiv \begin{pmatrix} 1 \\ 0 \end{pmatrix} \quad (23)$$

Also after easy calculation, we get

$$W^T D F_r E_0 V = 1 \neq 0 \text{ and}$$

$$W^T D^2 F_r E_0(V, V) = \frac{-2r}{k} - 2d_1 \neq 0$$

So a transcritical bifurcation occurs around $E(0, 0)$.

(2) At $E_1(x_1, 0)$

let V and W are eigen vector corresponding to zero eigen value of $J(E_1)$ and $J(E_1)^T$ respectively, where

$$V = \begin{pmatrix} v_1 \\ v_2 \end{pmatrix} \equiv \begin{pmatrix} 1 \\ 0 \end{pmatrix} \quad (24)$$

Similarly we get

$$W = \begin{pmatrix} w_1 \\ w_2 \end{pmatrix} \equiv \begin{pmatrix} 1 \\ -\frac{Q_1}{Q_2} \end{pmatrix} \quad (25)$$

where

$$\begin{aligned} Q_1 &= -c_1 x_1 - \frac{c_2 x_1}{a + x_1} \\ Q_2 &= m c_1 x_1 + \frac{m c_2 x_1}{a + x_1} - d - q_2 E \end{aligned} \quad (26)$$

$$F_r E_1 = \begin{pmatrix} x_1 - \frac{(x_1)^2}{k} \\ 0 \end{pmatrix}$$

and we get

$$\begin{aligned} W^T F_r E_1 &= x_1 - \frac{(x_1)^2}{k} \\ W^T D F_r E_1 V &= 1 - 2 \frac{x_1}{k} \\ W^T D^2 F_{E_1}(V, V) &= -2 \frac{r}{k} - 2d_1 \end{aligned} \tag{27}$$

Therefore we get if $x_1 = k$ and $x_1 \neq \frac{k}{2}$, then transcritical bifurcation occurs at predator free equilibrium $E_1(x_1, 0)$, and if $x_1 \neq k$ then saddle node bifurcation occurs at $E_1(x_1, 0)$. \square

5.2 Existence and stability of Hopf bifurcation

At $E^*(x^*, y^*)$ if

- (a) $tr(J_{E^*}) = 0$
- (b) $det(J_{E^*}) > 0$
- (c) $\frac{d}{dr} tr(J_{E^*}) \neq 0$

then the system undergoes a hopf bifurcation at interior equilibrium point.

So if

- (a) $M_{11} + M_{22} = 0$
- (b) $M_{11}M_{22} - M_{12}M_{21} > 0$
- (c) $x^* \neq \frac{k}{2}$

then the system undergoes a hopf bifurcation. Now if $A > 0$ then the periodic orbit is unstable i.e the bifurcation is subcritical and if $A < 0$ then the periodic orbit is stable i.e the bifurcation is supercritical.

where

$$A = \frac{1}{16}(f_{xxx} + f_{xyy} + g_{xxy} + g_{yyy}) + \frac{1}{16w}[f_{xy}(f_{xx} + f_{yy}) - g_{xy}(g_{xx} + g_{yy}) - f_{xx}g_{xx} + g_{yy}f_{yy}]$$

Here

$$A = \frac{1}{16w}[d_1(c_1 + \frac{ac_2}{(a+x)^2}) + d_2(mc_1 + \frac{mac_2}{(a+x)^2})]$$

which implies that $A > 0$. So the hopf bifurcation is subcritical.

6 References